

# Differential Relations

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# Differential Motion and Statics



- ❑ Tool configuration and Joint Space velocity
- ❑ Jacobian
  - ❖ Tool configuration Jacobian
  - ❖ Manipulator Jacobian
- ❑ Singularity
  - ❖ Boundary Singularity
  - ❖ Interior Singularity
- ❑ Generalised Inverse
- ❑ Pseudo Inverse
- ❑ Statics
- ❑ Examples

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## Differential Relations

- Robot path planning problem is formulated in tool-configuration space

- Robot motion is controlled at the joint space

$x = w(q)$ ;  $x$  = tool configuration vector,  
 $w$  = tool-configuration function and  $q$  = joint variables

**Differential relationship**

$\dot{x} = J(q)\dot{q}$ ;  $J(q)$  is a  $6 \times n$  matrix and is called the Jacobian matrix

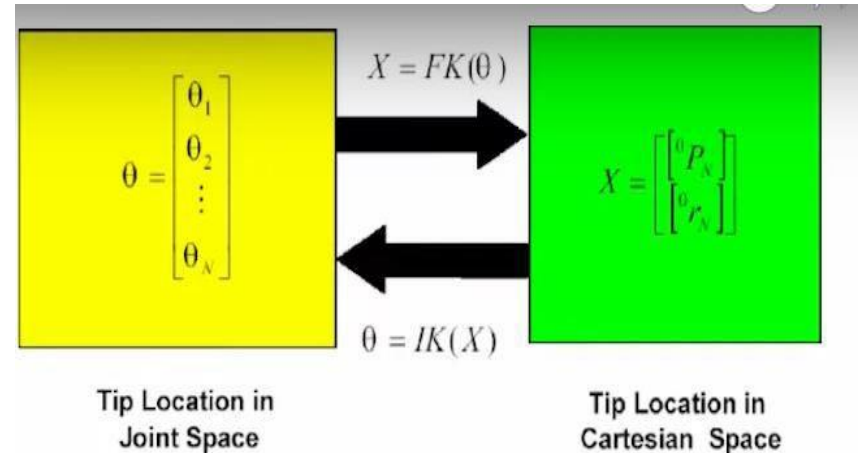
or Jacobian

$$J_{kj}(q) = \frac{\partial w_k(q)}{\partial q_j} \quad 1 \leq k \leq 6, \quad 1 \leq j \leq n$$

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$$\dot{X} = W \dot{q} \rightarrow$$

$$\begin{array}{c}
 \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \\ \dot{\omega}_x \\ \dot{\omega}_y \\ \dot{\omega}_z \end{bmatrix} \\
 6 \times 1
 \end{array}
 =
 \begin{array}{c}
 \begin{bmatrix}
 \frac{\partial w_1}{\partial q_1} & \frac{\partial w_1}{\partial q_2} & \frac{\partial w_1}{\partial q_3} & \dots & \frac{\partial w_1}{\partial q_n} \\
 \frac{\partial w_2}{\partial q_1} & \frac{\partial w_2}{\partial q_2} & \frac{\partial w_2}{\partial q_3} & \dots & \frac{\partial w_2}{\partial q_n} \\
 \frac{\partial w_3}{\partial q_1} & \frac{\partial w_3}{\partial q_2} & \frac{\partial w_3}{\partial q_3} & \dots & \frac{\partial w_3}{\partial q_n} \\
 \frac{\partial w_4}{\partial q_1} & \frac{\partial w_4}{\partial q_2} & \frac{\partial w_4}{\partial q_3} & \dots & \frac{\partial w_4}{\partial q_n} \\
 \frac{\partial w_5}{\partial q_1} & \frac{\partial w_5}{\partial q_2} & \frac{\partial w_5}{\partial q_3} & \dots & \frac{\partial w_5}{\partial q_n} \\
 \frac{\partial w_6}{\partial q_1} & \frac{\partial w_6}{\partial q_2} & \frac{\partial w_6}{\partial q_3} & \dots & \frac{\partial w_6}{\partial q_n} \\
 \frac{\partial q_1}{\partial q_1} & \frac{\partial q_2}{\partial q_2} & \frac{\partial q_3}{\partial q_3} & \dots & \frac{\partial q_n}{\partial q_n}
 \end{bmatrix} \\
 6 \times n
 \end{array}
 \begin{array}{c}
 \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \dot{q}_4 \\ \vdots \\ \dot{q}_n \end{bmatrix} \\
 n \times 1
 \end{array}$$

For a rotary manipulator,

$$\dot{x} = [J(\theta)] \dot{\theta}$$

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# Calculation of Jacobian

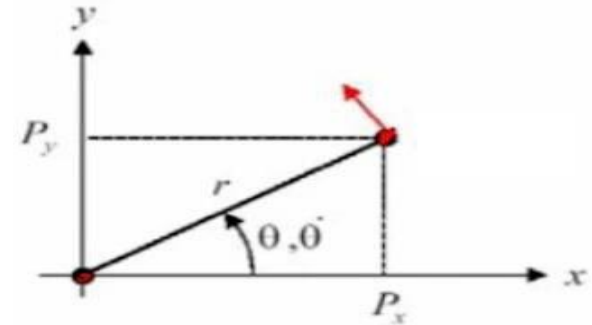
- Get the forward kinematics relationship,  $X=w(\theta)$
- Differentiate  $X$  wrt  $\theta$

## Example: Planar 1R Robot

The end effector position is given by

$$P_x = r \cos \theta$$

$$P_y = r \sin \theta$$



$$\begin{aligned} \dot{P}_x = \dot{x} &= -r \sin \theta \cdot \dot{\theta} \\ \dot{P}_y = \dot{y} &= r \cos \theta \cdot \dot{\theta} \end{aligned} \quad \Rightarrow \quad \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -r \sin \theta \\ r \cos \theta \end{bmatrix} \begin{bmatrix} \dot{\theta} \end{bmatrix}$$

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## Example: 3R Planar Manipulator

$$Px = l_1 C_1 + l_2 C_{12}$$

$$Py = l_1 S_1 + l_2 S_{12}$$

$$Pz = d_3$$

$$\begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} \frac{\partial p_x}{\partial \theta_1} & \frac{\partial p_x}{\partial \theta_2} & \frac{\partial p_x}{\partial \theta_3} \\ \frac{\partial p_y}{\partial \theta_1} & \frac{\partial p_y}{\partial \theta_2} & \frac{\partial p_y}{\partial \theta_3} \\ \frac{\partial p_z}{\partial \theta_1} & \frac{\partial p_z}{\partial \theta_2} & \frac{\partial p_z}{\partial \theta_3} \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix}$$

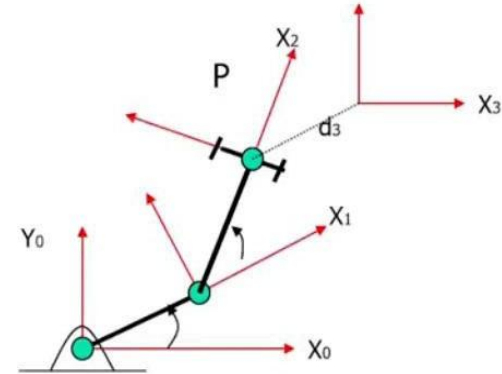
$3 \times 1 \quad \quad 3 \times 3 \quad \quad 3 \times 1$

$$J = \begin{bmatrix} -l_1 S_1 - l_2 S_{12} & -l_2 S_{12} & 0 \\ l_1 C_1 + l_2 C_{12} & l_2 C_{12} & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

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$$T_{base}^{tool} = \begin{bmatrix} C_{123} & -S_{123} & 0 & l_1 C_1 + l_2 C_{12} \\ S_{123} & C_{123} & 0 & l_1 S_1 + l_2 S_{12} \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Singularities

The joint space velocity is given as

$$\dot{\theta} = [J(\theta)]^{-1} \dot{x}$$

One of the potential problems with solving for joint space velocity is the non-existence of inverse. The Jacobian may not be invertible for all the values of  $\theta$ .

At certain points in joint space, Jacobian loses its rank; i.e. there is a reduction in no. of independent rows and columns. The points at which the Jacobian loses rank are called Joint space Singularities.

NOTE: The Jacobian Matrix  $J(q)$  is of full rank as long as  $q$  is not a joint space singularity.

Manipulator dexterity,  $\text{dex}(q) = \det[J^T J]$   $n \leq 6$

For the general case  $n \leq 6$ , the tool Jacobian matrix is less than full rank if and only if the  $n \times n$  matrix  $J^T J$  is singular.

For redundant manipulators ( $n > 6$ ), determinant of the  $6 \times 6$  matrix,  $J J^T$  must be used.

A manipulator is at joint space singularity if and only if  $\text{dex}(q) = 0$ .

Boundary singularities occur on the smooth surface of the work envelope.

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## Boundary Singularities of SCARA

$$J = \begin{bmatrix} -l_1 S_1 - l_2 S_{1-2} & -l_2 S_{1-2} & 0 & 0 \\ l_1 C_1 + l_2 C_{1-2} & l_2 C_{1-2} & 0 & 0 \\ 0 & 0 & -1 & 0 \end{bmatrix}$$

$$\begin{aligned} dex = \det(J^T J) &= (-l_1 S_1 - l_2 S_{1-2}) \cdot (-l_2 C_{1-2}) - l_2 S_{1-2} (l_1 C_1 + l_2 C_{1-2}) \\ &= l_1 l_2 (S_1 C_{1-2} - C_1 S_{1-2}) \\ &= l_1 l_2 S_2 \end{aligned}$$

$$dex() = 0 \text{ iff } S_2 = 0; \rightarrow \theta_2 = 0, \pi$$

When  $\theta_2 = 0$ , the arm is fully stretched and the tip is on the surface of the work envelope.

**Interior Singularity:** Potentially troublesome; formed when two or more axes form a straight line. The effects of rotation about one axis may be cancelled due to a counteracting rotation about the other axis. Tool configuration may remain the same even though the robot moves in joint space.

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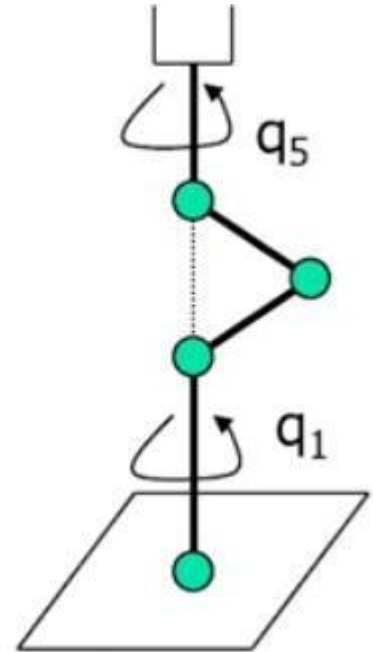
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## Example: Microbot-Alpha2

Consider the following locus of points in Joint space

$$q(\beta)=[q_1, -\beta, 2\beta-\pi, -\beta, q_5] \quad 0 < \beta < \pi/2$$

If  $a_3=a_2$  and  $a_4=0$ , then  $J(q)$  loses full rank along the line  $q=q(\beta)$  and  $q(\beta)$  represents interior singularities for the articulated robot.



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## Generalised Inverse

$$\dot{\theta} = [J(\theta)]^{-1} \dot{x}$$

Generalised Inverse: If  $A$  is an  $m \times n$  matrix, then an  $n \times m$  matrix  $X$  is a generalised inverse of  $A$  if and only if it satisfies at least property 1 or 2 of the following list of properties:

1.  $AXA = A$
2.  $XAX = X$
3.  $(AX)^T = AX$
4.  $(XA)^T = XA$

Most well known generalised Inverse is Moore-Penrose Inverse or **Pseudo Inverse ( $A^+$ )** which satisfies all 4 properties. If  $A$  is of full rank then,

$$\begin{aligned} A^+ &= A^T (AA^T)^{-1} & m \leq n \\ &= A^{-1} & m = n \\ &= (A^T A)^{-1} A^T & m \geq n \end{aligned}$$

## Example:

Find the pseudo Inverse of

$$A = \begin{bmatrix} 1 & 0 & 2 \\ 1 & -1 & 0 \end{bmatrix}$$

The rank of A is 2.

$$A^+ = A^T (AA^T)^{-1}$$



$$A^+ = \frac{1}{9} \begin{bmatrix} 1 & 4 \\ 1 & -5 \\ 4 & -2 \end{bmatrix}$$

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# Thank you!

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